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# Organo-functionalized MoS<sub>2</sub> as a nanofiller to enhance and control the swelling behavior of polybutadiene rubber nanocomposites



Rodrigo Fiel<sup>a,\*</sup>, Ingrid D. Barcelos<sup>b</sup>, Edson Roberto Leite<sup>a,c,\*\*</sup>

<sup>a</sup> Chemistry Department, Federal University of Sao Carlos, Sao Paulo, Brazil

<sup>b</sup> Brazilian Synchrotron Light Laboratory (LNLS), Brazilian Center for Research in Energy and Materials (CNPEM), Zip Code 13083-970, Campinas, Sao Paulo, Brazil

<sup>c</sup> Brazilian Nanotechnology National Laboratory (LNNano), Brazilian Center for Research in Energy and Materials (CNPEM), Campinas SP, Brazil

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Keywords: MoS <sub>2</sub> functionalization Rubber nanocomposites Swelling behavior	The functionalized MoS <sub>2</sub> (f-MoS <sub>2</sub> ), synthesized at different temperatures, was incorporated in polybutadiene (PB) rubber as a nanofiller and then vulcanized with sulfur without any further additives. The incorporation of f-MoS <sub>2</sub> into PB matrix promotes significant improvements in swelling properties that can be even compared to traditional fluorocarbon (FKM) and nitrile (NBR) rubbers. Moreover, the statistical results showcase that is possible to modulate the swelling behavior of the rubber nanocomposite by varying the amount of PB grafted on f-MoS <sub>2</sub> .

#### 1. Introduction

High-performance rubber nanocomposites have attracted attention owing to their wide range of applications which combines the viscoelastic properties of rubbers with the functionality of several types of reinforcing nanofillers [1–7]. Currently, the research on developing novel nanofillers becomes imperative in order to enhance the thermal, mechanical, swelling and processing properties as well as to overcome the environmental drawbacks caused by carbon black, which is the most used filler in the rubber industry [8].

Over the years, two-dimensional  $MoS_2$  has emerged as a potential nanofiller candidate to be incorporated in rubbers [9] because of its high Young's modulus (0.3 TPa) [10] allied with fascinating properties in catalysis [11], sensors [12,13], and field-effect transistors [14,15]. However, a homogeneous dispersion of  $MoS_2$  in polymeric matrices cannot be easily achieved using traditional blending techniques due to the lack of reactive groups and poor interaction with solvents of most of polymer matrices [16]. A further step towards enhancing the  $MoS_2$ dispersion is by surface functionalization with covalent or non-covalent ligands [17,18]. For instance, recent advances have been reported on  $MoS_2$  functionalized with organic thiol ligands (non-covalent) [19], diazonium salts (covalent) [20], and different polymers (covalent/non-covalent) [21]. Typically, rubbers are cross-linked polymers able to absorb a large amount of solvent without dissolving [22] and the incorporation of functionalized  $MoS_2$  in these types of polymers

represents a growing field of applications due to the excellent swelling control and enhanced mechanical properties [23,24]. In this context, polybutadiene (PB) rubber, an example of cross-linked polymer [25,26], is an interesting prototype to investigate the effects induced by functionalized MoS<sub>2</sub> on its structure. PB is present as a copolymer with nitrile or styrene resulting, respectively, in nitrile-butadiene rubber (NBR) and styrene-butadiene rubber (SBR), which are the most important commercial rubbers due to its widespread industrial applications [27]. The investigation of swelling-ratio on novel rubbers nanocomposites is essential to determine its structure [28] and potential industrial applications (i.e. automotive, aerospace, oil and gas, etc.) [29]. Apart from fluorocarbon rubber (FKM), which exhibits outstanding chemical resistance, traditional rubbers (i.e. PB, SBR and NBR) are usually nonresistant to organic solvents, certain types of oils and greases which impair their properties and the effects are undesirable in most applications. However, as it is known, the fabrication of FKM is difficult and expensive, leading to the development of new functional rubbers with high chemical resistance (low swelling-ratio) for advanced applications [30, 31].

In this communication,  $MoS_2$  was functionalized with PB (f-MoS<sub>2</sub>) via single-step liquid-phase exfoliation (LPE) process using ultrasonic bath at different temperatures following the protocol that we previously reported [32]. Here, we noticed that is possible to control the concentration of PB grafted on the edge sites of  $MoS_2$  by controlling the ultrasound bath temperature. Moreover, the f-MoS<sub>2</sub>s nanofiller were

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<sup>\*</sup> Corresponding author.

<sup>\*\*</sup> Corresponding author. Chemistry Department, Federal University of Sao Carlos, Sao Paulo, Brazil. E-mail addresses: rodrigospfiel@gmail.com (R. Fiel), edson.leite@lnnano.cnpem.br (E.R. Leite).



**Fig. 1.** a) Photograph of f-MoS<sub>2</sub> colloidal dispersions in toluene: f-MoS<sub>2</sub>T15, f-MoS<sub>2</sub>T30 and f-MoS<sub>2</sub>T60. b) Raman spectra of bulk-MoS<sub>2</sub> (black), f-MoS<sub>2</sub>T15 (red), f-MoS<sub>2</sub>T30 (blue) and f-MoS<sub>2</sub>T60 (green). (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)



**Fig. 2.** XRD diffractogram of bulk-MoS<sub>2</sub> (black) and the respective f-MoS<sub>2</sub>: f-MoS<sub>2</sub>T15 (red), f-MoS<sub>2</sub>T30 (blue), and f-MoS<sub>2</sub>T60 (green). (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

incorporated in different loadings in PB and then vulcanized only with sulfur, without any further additives, resulting in f-MoS<sub>2</sub>/PB rubber nanocomposites that showed significant improvements on the reduction of swelling ratio compared to neat PB and traditional commercial rubbers (i.e. FKM and NBR) in toluene and methyl-ethyl ketone (MEK). The results indicated that the swelling behavior of the f-MoS<sub>2</sub>/PB is governed by the amount of PB functionalized onto MoS<sub>2</sub> surface. Our findings provide new insights into improving swelling control in rubber induced by functionalized layered materials without using carbon black in its composition.

### 2. Results and discussion

We start the discussion by performing the morphological and structural characterization of the materials obtained. Fig. 1a shows that f- $MoS_2$  synthesized at 15 °C (f- $MoS_2T15$ ), 30 °C (f- $MoS_2T30$ ) and 60 °C (f- $MoS_2T60$ ) have high colloidal stability after six days in the ultrasonic bath (See Materials and Methods in SI). It is expected that the temperature plays an important role in LPE methods [33,34], inducing modification of the materials properties and solution concentration [35]. Fig. 1b shows the Raman spectra collected for bulk  $MoS_2$  and f- $MoS_2s$ . The frequency difference between  $E_{2g}^1$  and  $A_{1g}$  is 26.5 cm<sup>-1</sup> for bulk-MoS<sub>2</sub>, as expected for non-exfoliated material [36]. For f-MoS<sub>2</sub>s, the frequency difference ranged from 24.8 to 25.5 cm<sup>-1</sup>, indicating a high degree of exfoliation (~4–10 layers) [37]. Note that the frequency difference decreases when f-MoS<sub>2</sub> is synthesized at higher temperatures (i. e. f-MoS<sub>2</sub>T60), corroborating to the fact that the higher the temperature during the LPE process, the thinner are the exfoliated flakes obtained [33,34]. This is also in agreement with our AFM analysis. The line profile analysis obtained by AFM shows f-MoS<sub>2</sub> sheets ranging from ~5.5 nm (f-MoS<sub>2</sub>T60) to ~7.0 nm (f-MoS<sub>2</sub>T15) of height, which is equivalent to 7–9 layers [38] (See Figure S1a-c, SI). Furthermore, UV–visible spectra (Figs. S2 and SI) show the characteristics A and B excitonic absorption bands at 612 nm and 674 nm, respectively, which also indicates the exfoliation of MoS<sub>2</sub> [39].

The diffractogram of bulk  $MoS_2$  in Fig. 2 showed all characteristic peaks expected for this material corresponding (002), (004), (100), (103), (006), and (105) planes. The diffractogram of f-MoS<sub>2</sub> showed the absence of all peaks except the peak corresponding to the basal plane (002) that indicates the exfoliation of the sheets. The presence of only (002) plane suggests restacking of the functionalized sheets on the substrate during the drying process. The restacking has been reported in several works, mainly in the process involving lithium intercalation [40]. SEM images reveal that f-MoS<sub>2</sub>s are morphologically different from the bulk  $MoS_2$  [41] (See Figure S3-S5, SI) and the functionalized nanosheets are randomly oriented. In addition, it is possible to verify the random stacking corroborating with the diffraction patterns in Fig. 2 [42]. AFM and SEM images also show flakes with a lateral size smaller than 1.0  $\mu$ m and few surface defects.

The electronic structure and the interaction between MoS<sub>2</sub> and PB chains were studied by TEM and XPS. The representative TEM image (See Figure S6a-c, SI) shows several f-MoS<sub>2</sub> flakes electron transparent indicating a high degree of exfoliation which agrees with Raman measurements. After the deconvolution process, the XPS spectra of Mo3d show the 226.2eV peak referring to the S2s of  $S^{-2}$ , 229.4eV and 232.6eV peaks corresponding to Mo-S bonds of Mo<sup>4+</sup> 3d<sub>5/2</sub> and Mo<sup>4+</sup> 3d<sub>3/2</sub>, respectively [43]. Furthermore, it was able to identify the 233.7eV and 236.2eV corresponding to Mo–O bonds of  $Mo^{6+} 3d_{5/2} e Mo^{6+}3d_{3/2}$ , respectively [43]. The partial oxidation of MoS<sub>2</sub> is due to the oxidative mechanism in LPE process [35] (See Figs. S7a-c). Next, to verify the chemical interaction between PB and MoS<sub>2</sub> flakes, carbon C1s peaks were evaluated (Figs. S8a-c). The analysis of C1s peaks of neat PB showed C=C, C-C, and C-H bonds as expected. However, the analysis of f-MoS<sub>2</sub>s showed a complex set of C1s peaks after the deconvolution process. We identified peaks at 286.6eV and 288.7eV, indicating C-C-S and C-S bonds, respectively, regardless of the synthesis temperature [44]. The sulfur S2p of f-MoS<sub>2</sub> also suggests the presence of S-C peaks at 164.8eV (See Figs. S9a-c) [45]. Therefore, our analysis suggests that the functionalization occurs regardless of synthesis temperature.

Thermogravimetric analysis (TGA) (Figs. S10 and SI) was performed in order to quantify the amount of PB present in f-MoS<sub>2</sub>s as well as to verify its correlation with the ultrasound bath temperature of the singlestep LPE method. Bulk MoS2 undergoes a thermal degradation at 377 °C with a weight loss of 12.68 wt% that we attribute to the loss of SO<sub>2</sub> during this thermal event [46]. The difference between the bulk MoS<sub>2</sub> curve and f-MoS<sub>2</sub>s represents, exclusively, the mass loss of the PB grafted on the MoS<sub>2</sub>. Thus, TGA curves indicated a PB concentration of 2.57 wt %, 6.68 wt%, and 7.60 wt% for f-MoS<sub>2</sub>T15, f-MoS<sub>2</sub>T30 and f-MoS<sub>2</sub>T60, respectively. The increase in PB concentration on MoS<sub>2</sub> (almost three-fold between 60 °C and 15 °C) may be due to cascade effects: initially, increasing temperature increases the sonication induced scission events. Then, the successive scissions in ultrasound bath leads to an increasing number of sulfur active edge sites of MoS<sub>2</sub> that interact with more PB chains [35,40]. Now, we focus our attention to the swelling behavior of f-MoS<sub>2</sub>/PB rubber nanocomposites (Figure S11a-j, SI). The swelling ratio depends on the nature of the additives, their



Fig. 3. Swelling-ratio curves of neat PB and f-MoS<sub>2</sub>/PB rubber nanocomposites as a function of nanofiller loading and its synthesis temperature: a) in MEK and b) in toluene.



Increasing f-MoS, synthesis temperature

Fig. 4. a) TEM image of f-MoS<sub>2</sub>T60/PB rubber at 40 wt%. Schematic illustrations of f-MoS<sub>2</sub>/PB nanocomposites: b) proposed interaction between PB matrix and f-MoS<sub>2</sub> and c) proposed interaction between PB matrix and f-MoS<sub>2</sub> synthesized under different ultrasound bath temperatures.

concentration/dispersion and processing [47]. Fig. 3a–b shows the swelling behavior of neat PB and f-MoS<sub>2</sub>/PB rubber nanocomposites in MEK and toluene, as a function of the f-MoS<sub>2</sub> loading (wt%) and its synthesis temperature.

One can see that for all samples there is a significant reduction on the swelling ratio with increasing the  $f-MoS_2$  loading or its synthesis

temperature (See Table S1 in SI). For instance, the f-MoS<sub>2</sub>T60/PB 40 wt % rubber nanocomposite, which presented the best result, swelled 3.26  $\pm$  2.72% in MEK (Figs. 3a) and 55.00  $\pm$  10.00% in toluene (Fig. 3b). The swelling of neat PB rubber was 56.22  $\pm$  3.00% in MEK (the first measurement is shown in Fig. 3a) and 637.00  $\pm$  53.00% in toluene (the first measurement is shown in Fig. 3b), respectively. The comparative

swelling test for NBR and FKM in MEK were 122.00  $\pm$  0.04% and 168.00  $\pm$  0.03%, respectively. In toluene, the swelling ratio for NBR and MEK were 61.00  $\pm$  0.007% and 8.00  $\pm$  0.028%, respectively. Note that even neat PB rubber had better swelling performance in MEK than NBR and FKM. This result may be ascribed to the polarity difference between MEK and PB: particularly, MEK is considered a polar solvent due to ketone function in its structure. On the other hand, PB is highly nonpolar rubber which hinders the rubber/solvent interaction. Both NBR and FKM have polar groups in its structure (i.e. acrylonitrile and fluorine) which facilitates the rubber/solvent interaction leading to higher swelling-ratio. TEM image (Fig. 4a) revealed a good compatibility and dispersion, even at 40 wt%, between f-MoS<sub>2</sub> nanofiller and PB matrix without signs of percolation. Therefore, the striking reduction in swelling ratio of the rubber nanocomposites must be a direct consequence of interfacial nanofiller/PB interaction in such a way that the swelling results can be compared to swelling of traditional FKM and NBR rubbers. Obviously, FKM presented a lower swelling ratio in toluene compared to f-MoS<sub>2</sub>T60/PB 40 wt% rubber nanocomposite. However, it is worth remembering that both FKM and NBR have several additives in its formulation, such as, zinc oxide, oils, plasticizers and, of course, carbon black (See rubber formulations in Tables S2 and S3, SI). Those additives were not used in this study in order to evaluate the effect of the nanofillers and its loadings on swelling behavior of rubber nanocomposites. Based on these results, we believe that the grafted PB, induced by MoS<sub>2</sub>, is acting as a cross-linking agent in the PB matrix that contributes for the great reduction on swelling ratio by reducing the free volume of PB rubber structure [48] (Fig. 4b). The reduction of free volume in rubber structure creates constrained regions [49] that hampers the penetration of the solvent in the polymeric matrix [50].

Through statistical analysis (See Tables S4 and S5 and statistical discussion in SI), our results in Fig. 3a-b indicate that the swelling properties of rubber nanocomposites depend on the nanofiller loading and its synthesis temperature. Clearly, it is expected a reduction on swelling ratio as nanofiller loading increase because the interactions between nanofiller/PB will increase, reducing the free volume. According to swelling ratio curves in Fig. 3a-b and the data in Table S1 (See SI), as the f-MoS<sub>2</sub> synthesis temperature increase, at constant nanofiller loading, we noticed a reduction of the swelling ratio of the rubber nanocomposites. In this case, we believe that the effect of synthesis temperature on swelling behavior is intimately correlated with LPE exfoliation mechanism [35,40] which increases the amount of PB functionalized on the edge sites of f-MoS<sub>2</sub> calculated by TGA. Therefore, increasing the grafted PB concentration will interact more efficiently with PB matrix creating more constrained regions compared to the same f-MoS<sub>2</sub> synthesized at lower temperatures (Fig. 4c).

## 3. Conclusion

In summary, functionalized f-MoS<sub>2</sub> nanofillers were synthesized through single-step LPE at different ultrasound bath temperatures. The incorporation of f-MoS<sub>2</sub> in PB rubber without any further additives promoted significant enhancement on swelling properties that can be compared to traditional commercial rubbers (namely FKM and NBR). This is an interesting result that turns f-MoS<sub>2</sub> nanofiller as a great candidate to replace carbon black in rubber formulations. Moreover, through statistical analysis (See SI), we noticed a direct and independent correlation between the synthesis temperature of nanofiller and its loading in a PB matrix on the reduction of the swelling ratio. Thus, we were able to modulate the amount of absorbed solvent with nanofiller loading or its temperature of synthesis. Finally, the results showed that the enhancement on swelling property is due to the good interface interaction between grafted PB in f-MoS2 and PB matrix reducing the free volume in rubber nanocomposite structure. The f-MoS2 nanofiller opens new opportunities for the development of novel and functionalized materials with superior swelling characteristics and controlled chemical resistance.

# CRediT authorship contribution statement

**Rodrigo Fiel:** Conceptualization, Methodology, Investigation, Writing – original draft, Investigation, Data curation, Validation. **Ingrid D. Barcelos:** Writing – review & editing, Visualization, Supervision, Formal analysis. **Edson Roberto Leite:** Supervision, Project administration.

# Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.coco.2021.101053.

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